

Estimation of Building Parameters Using Simplified Energy Balance Model and Metered Whole Building Energy Use

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Hiroko Masuda and Dr. David E. Claridge
Energy Systems Laboratory, TEES
Texas A&M University



Texas A&M University, College Station, TX, USA



Manchester, UK

Background

Energy use analysis for Texas A&M University campus buildings

- Assessment of daily data from 520 energy meters for electricity, chilled water, and heating water in 171 buildings (16,000,000 ft² or 1,500,000 m²) every month
 - Anomaly detection, imputation of missing data, estimation of appropriate consumption for unreliable meters
 - Billing information for utilities department
 - Monitoring changes in the consumption patterns and levels
 - Track energy performance after energy retrofit
 - Detect opportunities for energy use optimization

Background

- Energy balance variable (Shao and Claridge, 2006)
 - Applications for energy data analysis (Baltazar et al., 2007 and 2012)

Whole building control volume

$$\Delta E_{CV} = E_{entering} - E_{leaving}$$

$$= Q_{air} + Q_{cond} + Q_{sol} + Q_{occ} + \overbrace{Q_E - E_C + E_H}^{\text{Measurable}}$$

Steady state $\Delta E_{CV} = 0$

$$E_{BL} = Q_E - E_C + E_H$$

$$= fE_E - E_C + E_H$$

$$= -Q_{air} - Q_{cond} - Q_{sol} - Q_{occ}$$

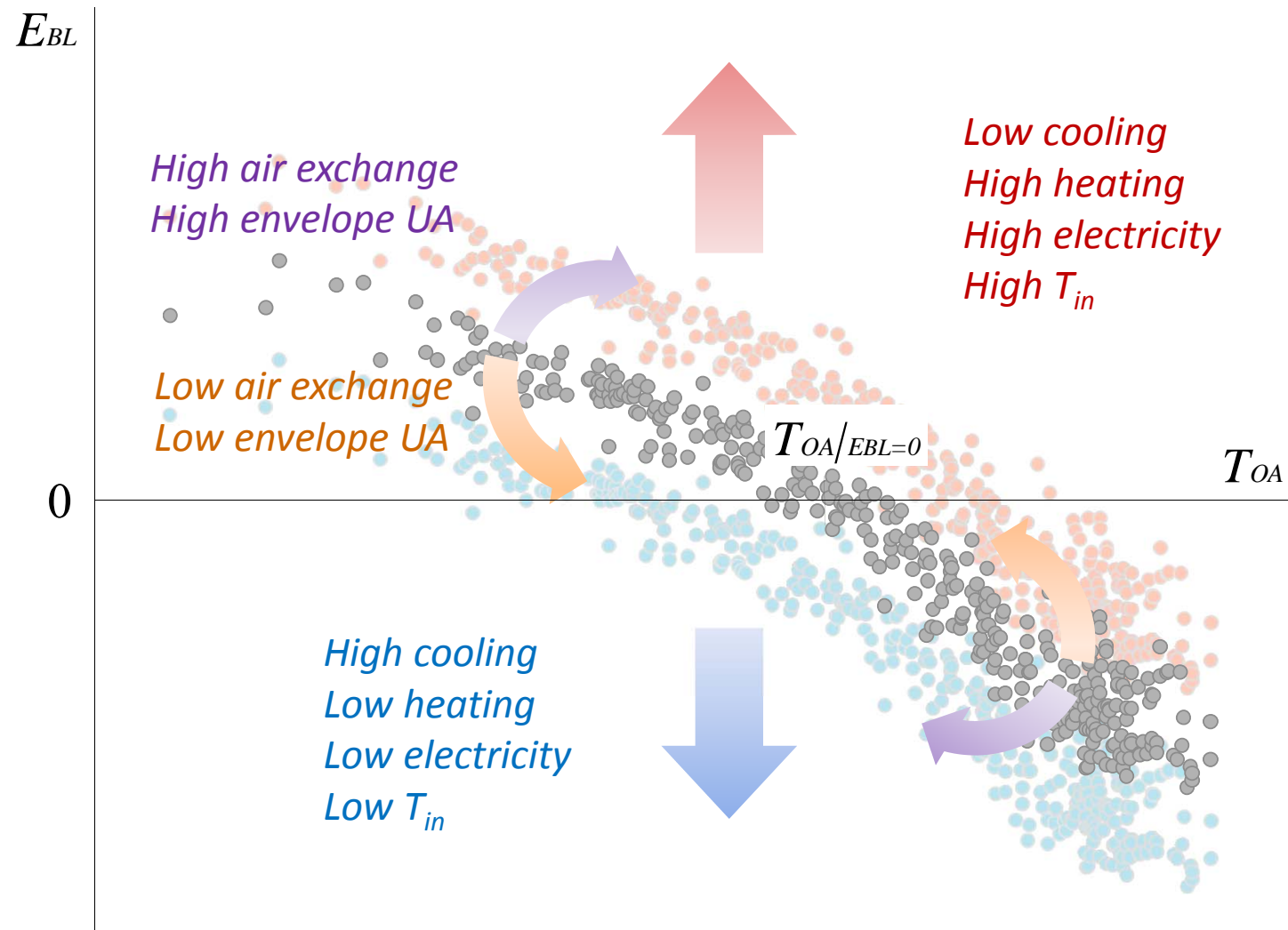
Heating energy use

Cooling energy use

Heat load from electricity use

Indirect measurement
of the aggregate load

Interpretation of Energy Balance



Motivation

- Quantify the interpretation of Energy Balance
 - Air exchange rates and overall heat loss coefficient of the building envelope have significant influences on the heating and cooling loads.
 - Direct measurement of those parameters in operating buildings requires considerable time and labor.
 - Obtained parameters can be used for building energy optimization.
 - Data validation technique can be refined.

Earlier studies on building parameter estimation (steady-state)

- Rabl and Rialhe (1992)
 - Cooling and heating energy consumption is separately analyzed.
 - Misleading parameter estimates for commercial buildings with simultaneous cooling and heating
- Reddy et al. (1994)
 - Building thermal load (Q_B)
 $Q_B = \text{cooling energy use} - \text{heating energy use}$
- Deng (1997)
 - Estimation of overall heat loss coefficient and ventilation parameter using the Q_B variable
 - Synthetic simulation energy use data with constant building parameters
 - The parameter estimates are found to be accurate when daily data over the entire year are used.

This study

- Develops steady-state models and expression of key parameters for E_{BL} . Revisits Q_B model expressions based on the whole building energy balance.
- Compares parameter estimations using E_{BL} models and Q_B models.
- Non-ideal case is also tested.
- Proposes a reference temperature parameter T_{in}^* as a measure to check unbalanced cooling and heating consumption or unreliable models.

Methodology

- Develop regression models
 - Simplified steady-state models for the E_{BL} and Q_B variables
 - Mathematical expressions of key parameters
- Estimate and evaluate parameters using multiple linear regression analysis.
 - Simulation building
 - Data
 - Energy Plus simulation model for a large commercial building
 - Compare parameter estimates with simulation inputs
 - Actual buildings
 - Data
 - Measured OA volume air flow from 3 buildings
 - Compare parameter estimates with measured values

Models

Energy balance load (E_{BL})

$$\begin{aligned} E_{BL} &= E_E - E_C + E_H \\ &= -Q_{air} - Q_{cond} - Q_{sol} - Q_{occ} + (1-f)E_E \end{aligned}$$

Building thermal load (Q_B)

$$\begin{aligned} Q_B &= E_C - E_H \\ &= Q_{air} + Q_{cond} + Q_{sol} + Q_{occ} + Q_E \\ &= Q_{air} + Q_{cond} + Q_{sol} + Q_{occ} + fE_E \end{aligned}$$

f = fraction of electricity use (E_E) which turns into the heat load ($0 \leq f \leq 1$)

Simplified steady-state loads

Air exchange $Q_{air} = m_v c_p (T_{oa} - T_{in}) + m_v h_v X (W_{oa} - W_{in})$

Conduction $Q_{cond} = UA_s (T_{oa} - T_{in})$

Solar $\begin{aligned} Q_{sol} &= a_{sol} + b_{sol} T_{oa} \\ &= a'_{sol} + b_{sol} (T_{oa} - T_{in}) \end{aligned}$

$$X = \begin{cases} 1 & (W_{oa} > W_{in}) \\ 0 & (\text{otherwise}) \end{cases}$$

$$\begin{aligned} W_{in} &\leq 0.01 \text{ kg/kg} \\ T_{in} &= \text{const.} \end{aligned}$$

$$Q_{occ} + fE_E = E_{LE} k_s (1 + k_l X)$$

Deng (1997)

Regression models

$$E_{BL} = \beta_0 + \beta_T T_{oa} + \beta_W X (W_{oa} - W_{in}) + \varepsilon$$

$$\begin{aligned} Q_B &= \beta_0 + \beta_{sens} E_{LE} + \beta_{lat} X E_{LE} \\ &\quad + \beta_T T_{oa} + \beta_W X (W_{oa} - W_{in}) + \varepsilon \end{aligned}$$

Key Parameters

Regression models

$$E_{BL} = \beta_0 + \beta_T T_{oa} + \beta_W X(W_{oa} - W_{in}) + \varepsilon$$

$$Q_B = \beta_0 + \beta_{sens} E_{LE} + \beta_{lat} X E_{LE} + \beta_T T_{oa} + \beta_W X(W_{oa} - W_{in}) + \varepsilon$$

$$X = \begin{cases} 1 & (W_{oa} > W_{in}) \\ 0 & (\text{otherwise}) \end{cases}$$

	Building parameter	E_{BL}	Q_B
Air exchange rate	m_v	$-\hat{\beta}_W / h_v$	$\hat{\beta}_W / h_v$
Overall heat transfer coefficient	$U^* A_s$	$-\hat{\beta}_T + \hat{\beta}_W c_p / h_v$	$\hat{\beta}_T - \hat{\beta}_W c_p / h_v$
Reference temperature	T_{in}^*	$-\hat{\beta}_0 / \hat{\beta}_T$	$-\hat{\beta}_0 / \hat{\beta}_T$

Reference temperature T_{in}^* is similar to the balance point temperature

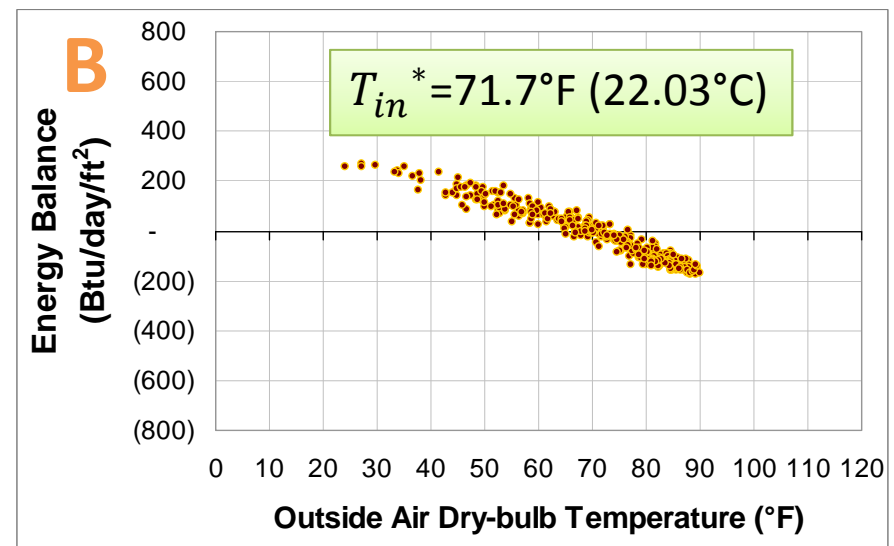
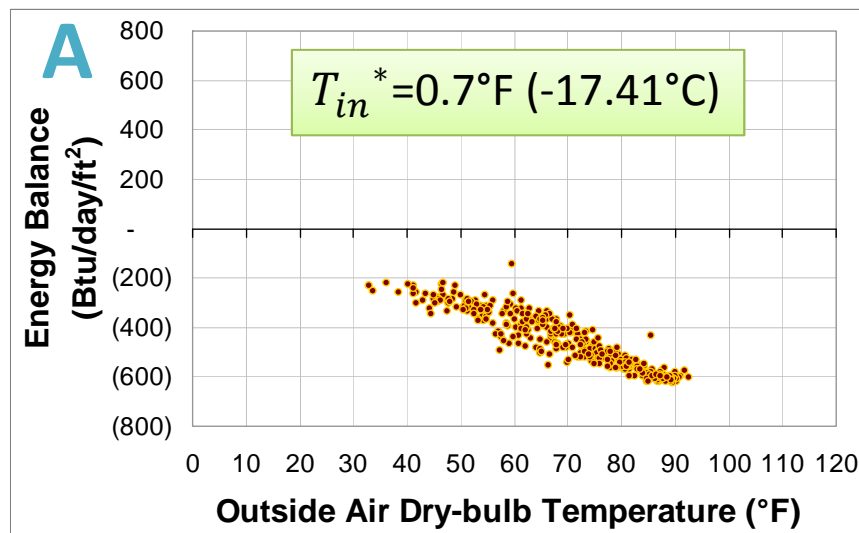
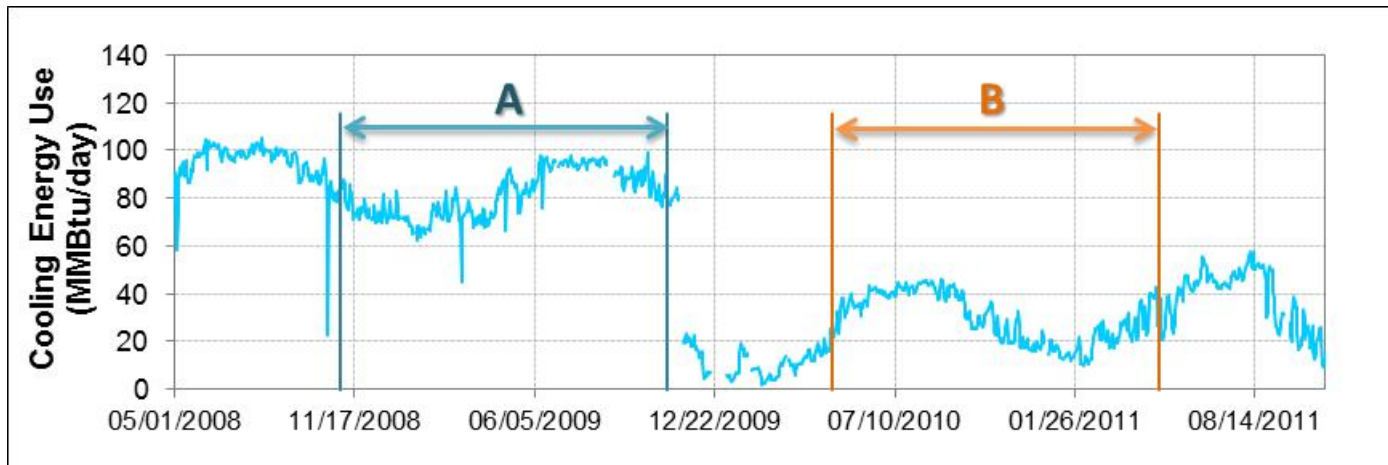
$$E_{BL} \quad T_{in}^* = T_{in} - \frac{Q_{occ} + a'_{sol}}{UA_s + m_v c_p + b_{sol}}$$

T_{in}^* for E_{BL} is typically 2°C to 3°C below T_{in}
(stable)

$$Q_B \quad T_{in}^* = T_{in} - \frac{a'_{sol}}{UA_s + m_v c_p + b_{sol}}$$

T_{in}^* for Q_B is around 1°C to 2°C below T_{in}
(depends on the model fitting)

Example of the use of T_{in}^*



Evaluation of Parameter Estimations

- Synthetic data from EnergyPlus building energy simulation
 - Results using daily data are shown here.
- Metered data from three campus buildings
 - Results from two buildings are shown here.

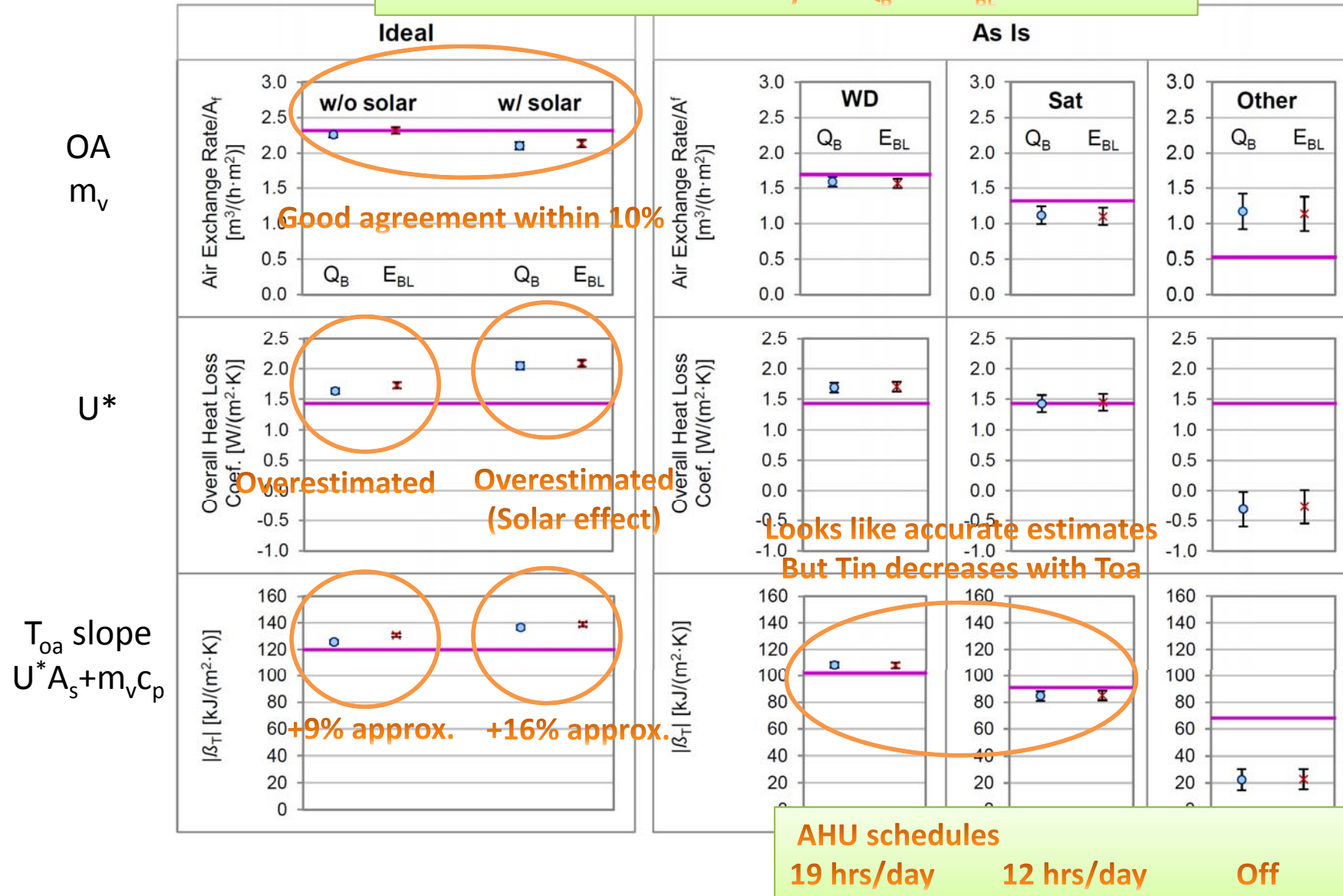
Energy use data from simulation - Data

Large commercial building in a hot and humid climate region

- The commercial reference building model for existing buildings constructed in or after 1980 in a hot and humid climate zone (DOE 2010)
- 12 stories above grade and a basement
- Total conditioned area of 46 320 m²
- Single duct VAV systems with reheat terminals
- No economizer or heat recovery
- Houston, TX TMY 2 weather data
- Three runs
 - **As is:** Original input file with many sources of energy use variability. Three different schedules for Weekday (WD), Saturday (Sat), and Sunday and holidays (Other); HVAC on/off; T_{in} variations due to set point reset
 - **Ideal w/ solar:** Constant indoor temperature set point and ventilation, HVAC is on all the time, no infiltration.
 - **Ideal w/o solar:** same simulation model as above but solar irradiance of the weather file was set to zero.

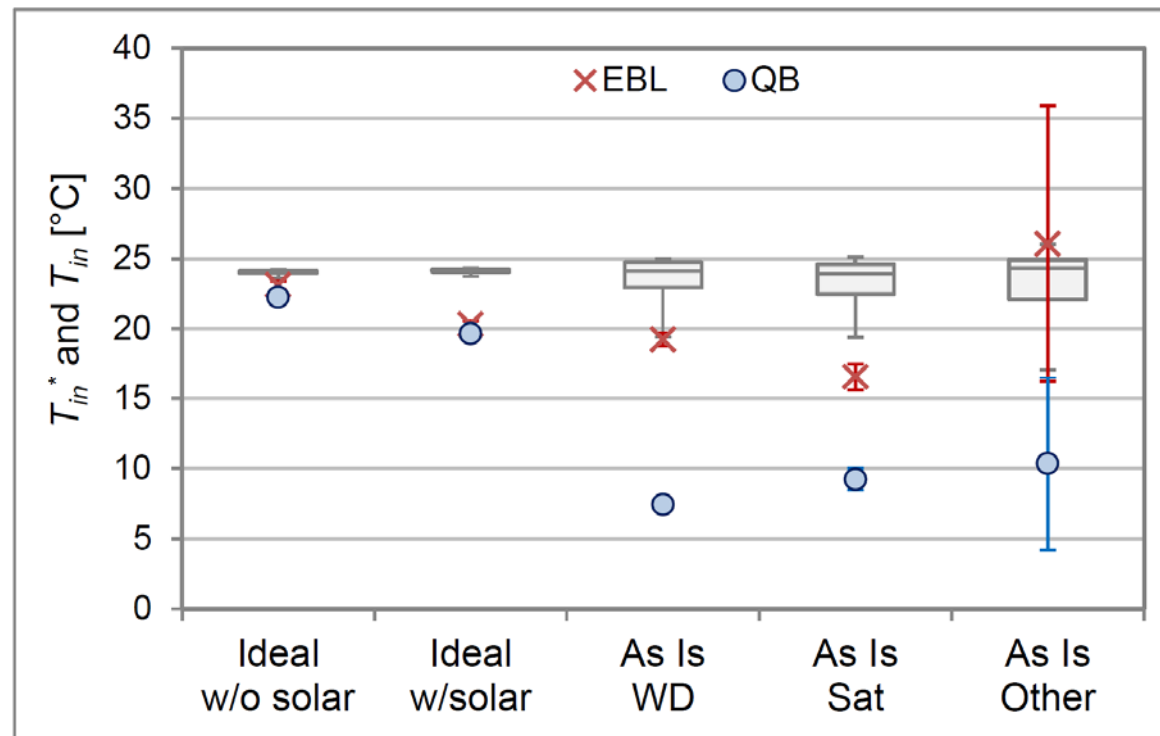
Energy use data from simulation – Results

Similar level of accuracy for Q_R and E_{RI} models



Energy use data from simulation – Results

Reference Temperature T_{in}^*



$$E_{BL} \quad T_{in}^* = T_{in} - \frac{Q_{occ} + a'_{sol}}{UA_s + m_v c_p + b_{sol}}$$

$$Q_B \quad T_{in}^* = T_{in} - \frac{a'_{sol} + Q_{occ} + fE_E}{UA_s + m_v c_p + b_{sol}}$$

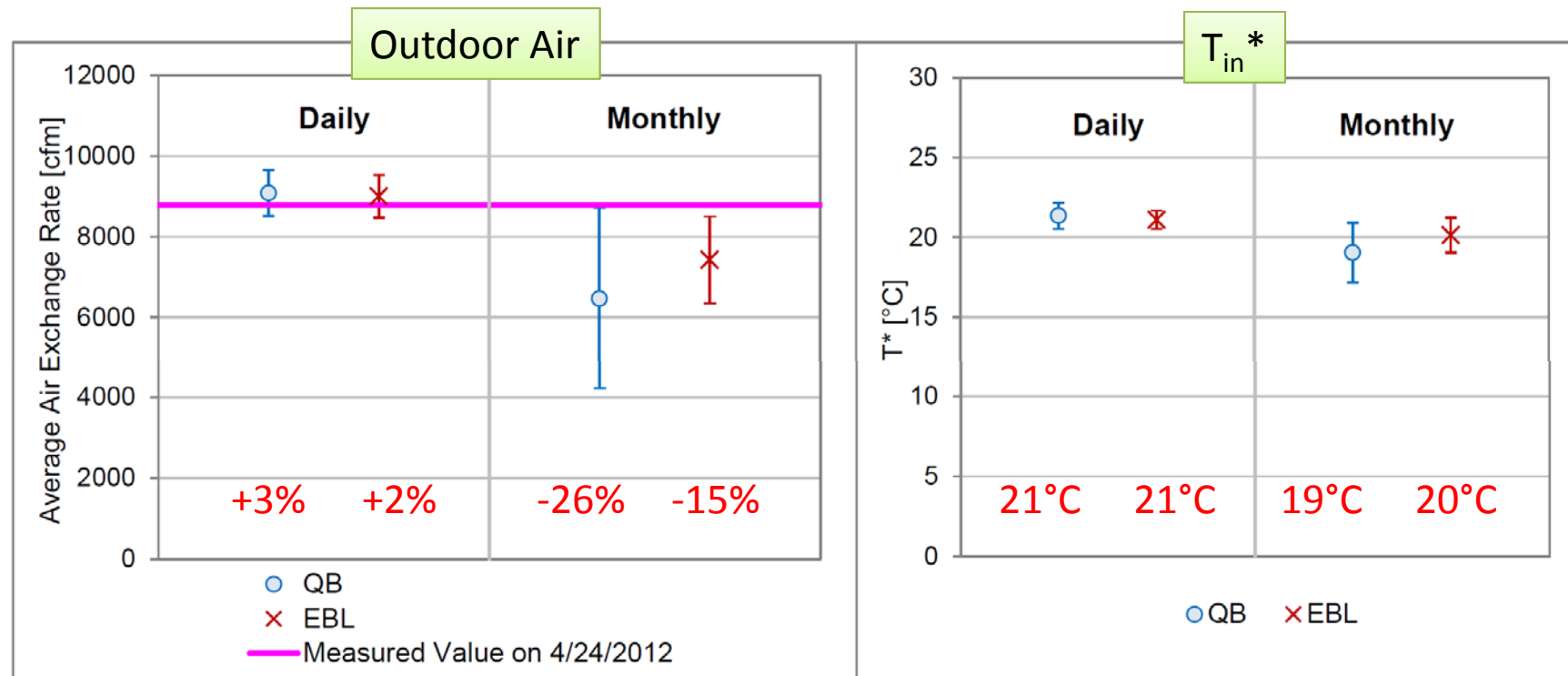
Energy use data from actual buildings

- Four-story dormitories ($\sim 6000 \text{ m}^2$)
- Similar design and dimensions built in 1979 and 1980.
- Dedicated outdoor air systems
 - OA flow rate was measured on 4/24/2012
- Local weather data
 - National Climatic Data Center
- Metered energy data
 - Bldg HS: 7/1/2011–6/30/2012
 - Bldg MF: 9/1/2011–6/30/2012
 - Bldg HB: 7/21/2011–6/30/2012



Energy use data from actual buildings-Results

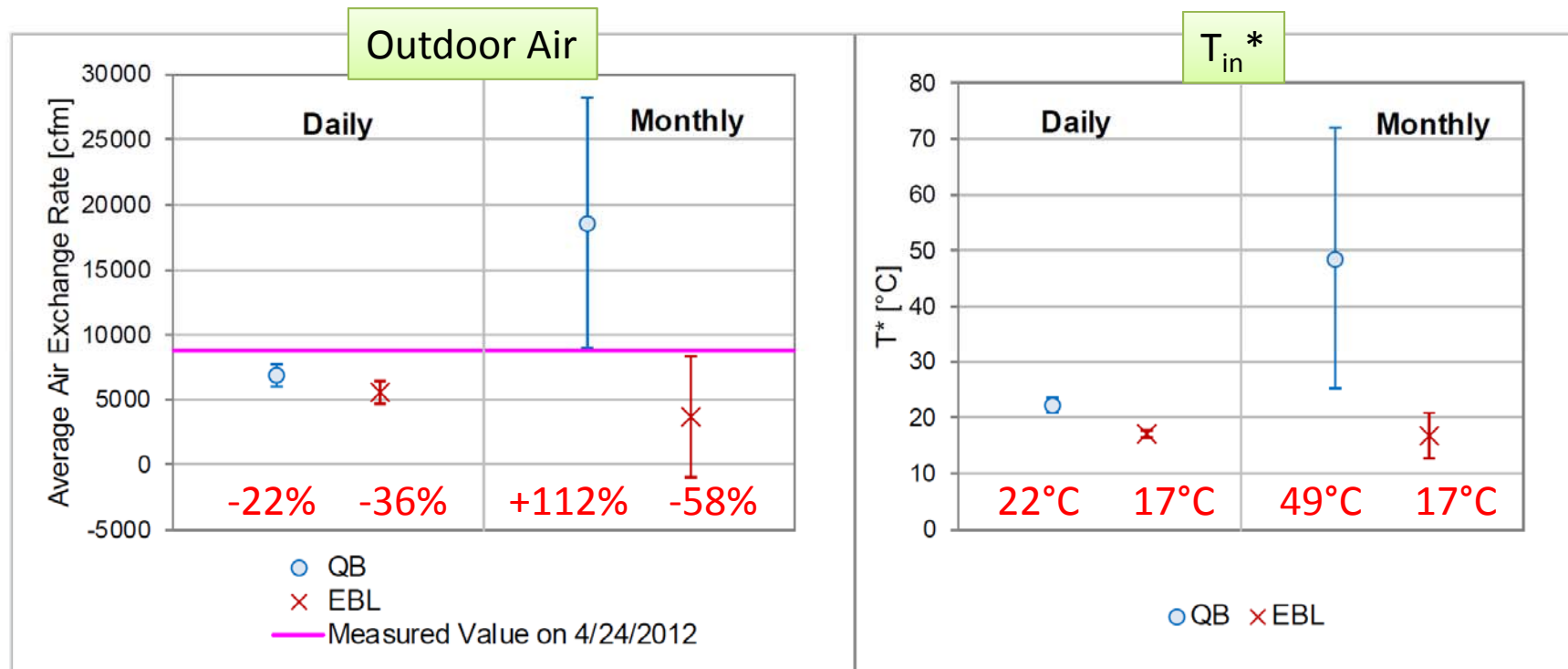
HS building



- Monthly data have stronger multicollinearity compared to daily data (VIF>10 for Q_B models and VIF>4 for E_{BL} models)

Energy use data from actual buildings-Results

HB Building



- OA flow rate changed during the modeling period.
- Questionable reference temperature T_{in}^*
- High collinearity between OA humidity and electricity variables in the Q_B monthly model. The effect of electricity variable is overestimated around 5 times as high as the normal level.

Summary and Future Studies

- Data-driven method to estimate influential building parameters using variables E_{BL} and Q_B have been presented.
- E_{BL} and Q_B models have a similar level of accuracy of the parameter estimates (daily synthetic data max. error: +10% for air exchange rate and -16% for T_{oa} slope), however, Q_B models require more careful selection of variables.
 - Latent portion of Q_{occ} doesn't have detectable relation with electricity use in real data.
 - Electricity variable is not suitable for grouped data by day types (small variability)
 - Electricity variable caused unexpected inflations of the estimates in the monthly data
- Parameters estimated under mild violations of model assumptions for the simulation data did not show serious errors.
 - 12 hrs/day HVAC operating hours
 - T_{in} set point reset (occupied/unoccupied hours, cooling/heating)
- A parameter T_{in}^* have introduced to detect problems in the metered energy data and model misspecifications.
- A dormitory building with stable parameters during the modeling period yielded +3% error (daily data) and -15% error (monthly data) in the air exchange rate estimates.
- How to set a reasonable range for T_{in}^* ?
- Is this method applicable to dry weather?

Thank you

References

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- Reddy, T. A., Deng, S., and Claridge, D. E. (1999). Development of an Inverse Method to Estimate Overall Building and Ventilation Parameters of Large Commercial Buildings. *Journal of Solar Energy Engineering*, 121, 40-46.
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- Shao, X. and Claridge, D.E. (2006). Use of first law energy balance as a screening tool for building energy data, part I - methodology. *ASHRAE Transactions* 2006, Vol. 112, Pt. 2 112:717-731.

Table 5: Data sets used in the analysis and the explanatory variable terms included in the regression models. The checked terms are included.

Dataset	Explanatory variable terms included in the regression models					
	E_{BL}		Q_B			
	T_{oa}	$X(W_{oa}-W_{in})$	T_{oa}	$X(W_{oa}-W_{in})$	E_{LE}	XE_{LE}
<i>Daily interval</i>						
Ideal w/ solar	✓	✓	✓	✓	✓	✓
Ideal w/o solar	✓	✓	✓	✓	✓	✓
As is (WD)	✓	✓	✓	✓		
As is (Sat)	✓	✓	✓	✓		
As is (Other)	✓	✓	✓	✓		
HS (Jul–Jun)	✓	✓	✓	✓	✓	
MF	✓	✓	✓	✓	✓	
HB	✓	✓	✓	✓	✓	
<i>Monthly interval</i>						
Ideal w/ solar	✓	✓	✓	✓	✓	
Ideal w/o solar	✓	✓	✓	✓	✓	
As is	✓	✓	✓	✓	✓	
HS (Jul–Jun)	✓	✓	✓	✓	✓	
MF	✓	✓	✓	✓	✓	
HB	✓	✓	✓	✓	✓	

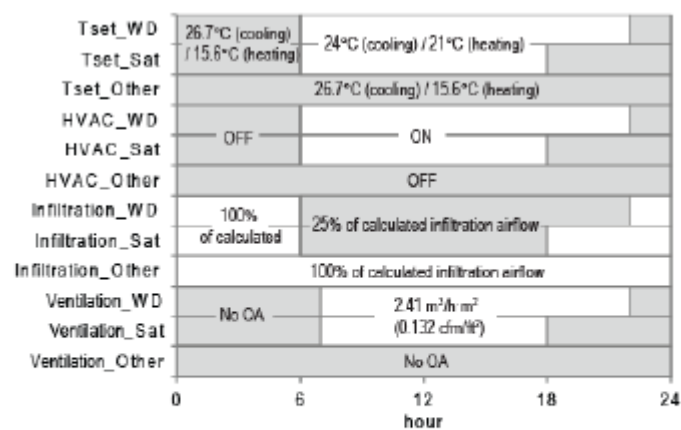


Fig. 1. System schedules for the as-is case

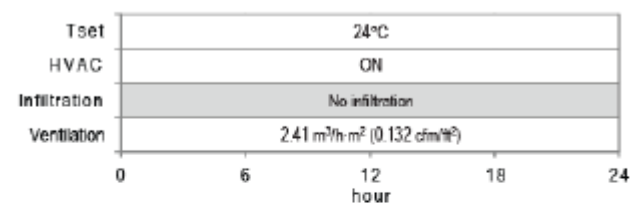


Fig. 2. System schedules for the ideal cases

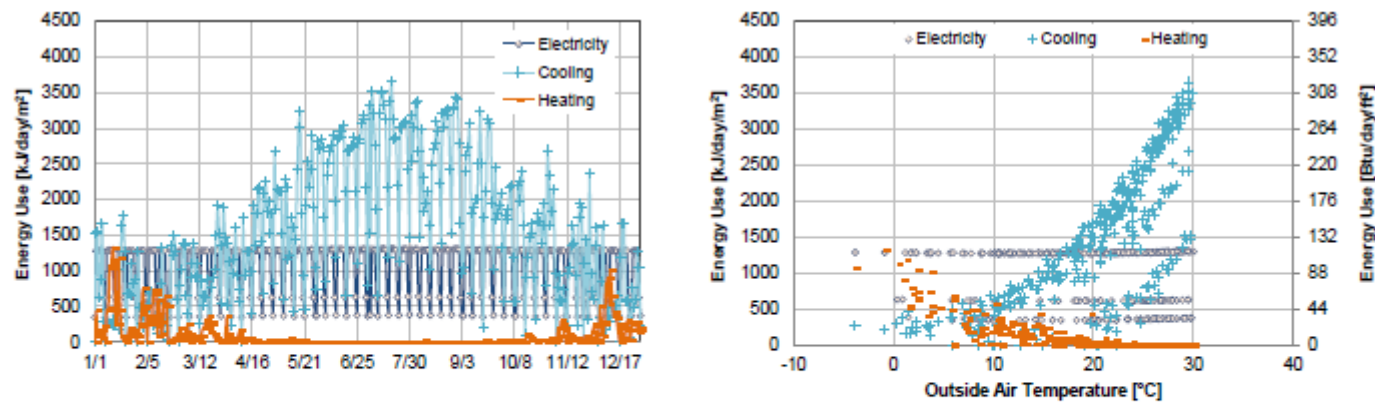


Fig. 3. Whole building daily energy uses for electricity, cooling, and heating per unit conditioned floor area for the as-is case. Time series plot is in the left and scatter plot versus daily average outside air temperature is in the right.

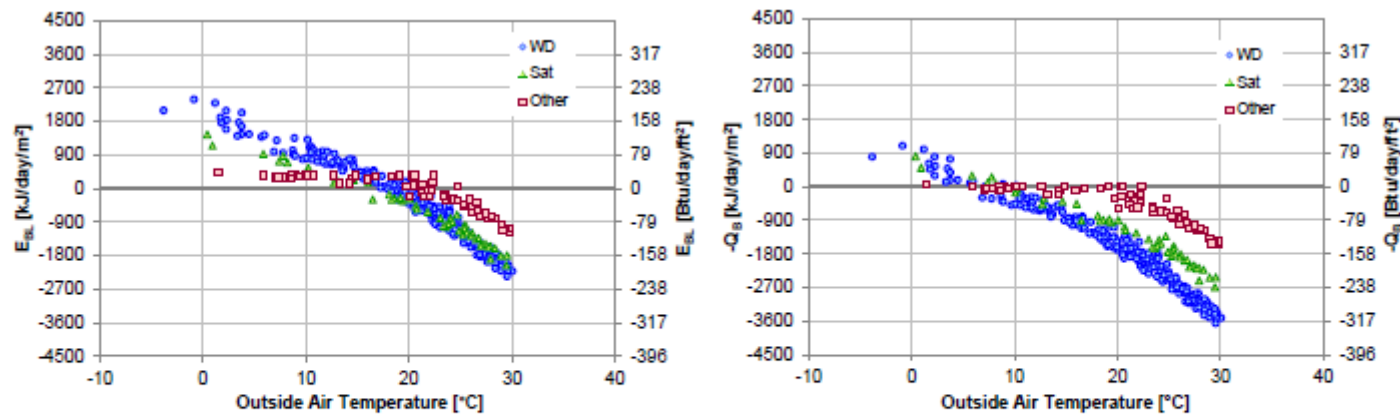


Fig. 4. E_{BL} and Q_B per unit conditioned floor area in the as-is case plotted versus daily average outside air temperature

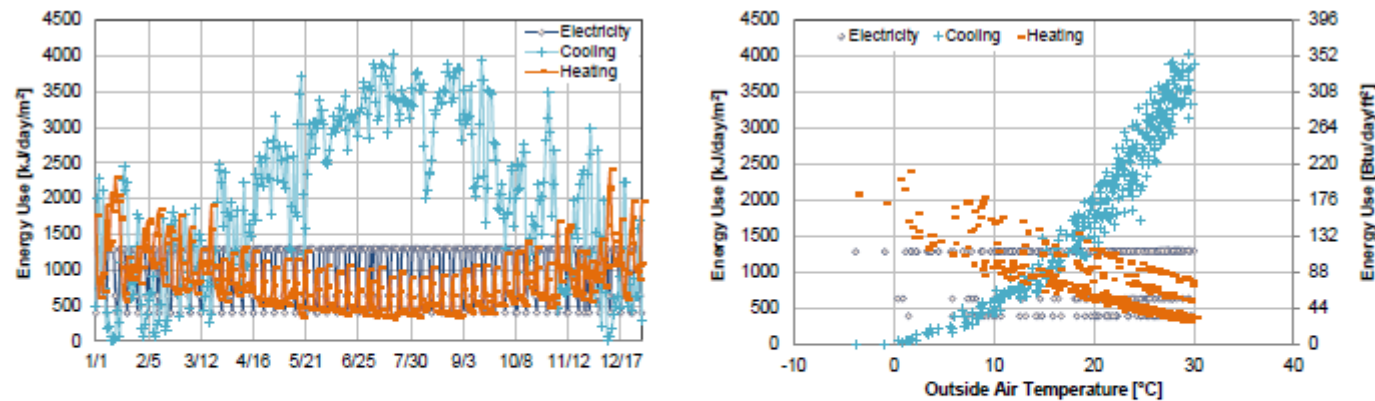


Fig. 5. Whole building daily energy uses for electricity, cooling, and heating per unit conditioned floor area for the ideal w/o solar case. Time series plot is in the left and scatter plot versus daily average outside air temperature is in the right.

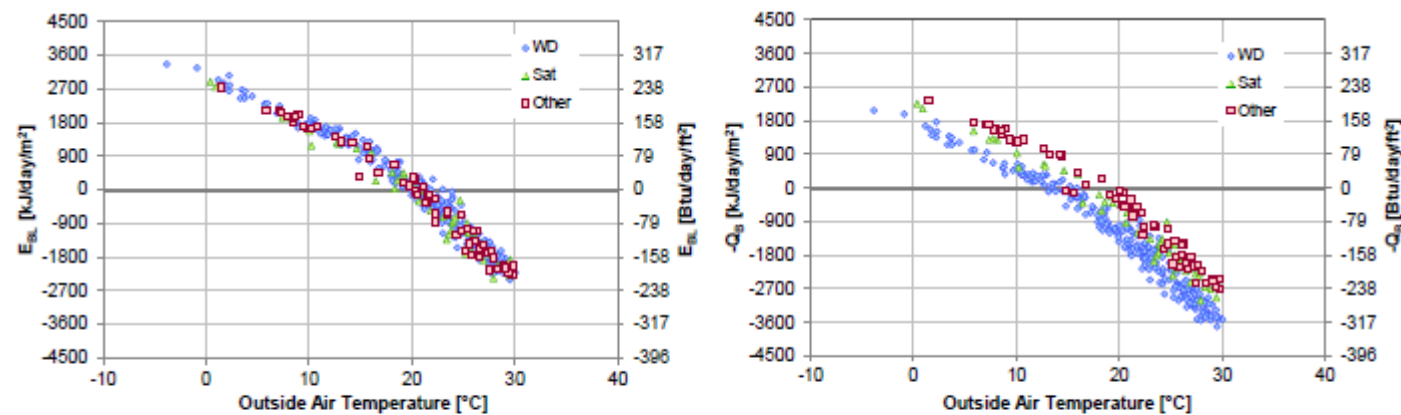


Fig. 6. E_{BL} and Q_B per unit conditioned floor area in the ideal w/o solar case plotted versus daily average outside air temperature.

$$VIF = \frac{1}{1 - R_i^2} \quad (12)$$

where R_i^2 is the multiple coefficient of determination between the i -th explanatory variable and all of the other explanatory variables in the regression equation. The exact value of VIF at which multicollinearity is declared depends on the individual investigator. Some use a value of 5 and others 10 (Haan, 2002).

Explanatory variable	Daily	Monthly	Daily	Monthly	Daily	Monthly	Daily WD	Daily Sat	Daily Other
T_{oa}	4.02	15.63	3.07	8.34	3.07	7.59	2.96	2.95	3.77
$X(W_{oa} - W_{in})$	3.15	8.12	3.08	7.94	3.07	7.59	2.96	2.95	3.77
E_{LR}	1.55	1.28	1.00	1.14					
XE_{LR}	2.97	5.97							

Explanatory variable	HS				MF				HB			
	Daily	Monthly	Daily	Monthly	Daily	Monthly	Daily	Monthly	Daily	Monthly	Daily	Monthly
T_{oa}	2.95	14.53	2.86	4.25	2.17	5.23	2.13	2.48	2.72	11.39	2.66	4.01
$X(W_{oa} - W_{in})$	3.16	15.28	2.86	4.25	2.33	5.52	2.13	2.48	2.96	21.51	2.66	4.01
E_E	1.13	3.69			1.11	2.33			1.15	6.19		